# DESIGNING TEMPORARY SOIL NAIL WALLS USING UNSATURATED SOIL SHEAR STRENGTH

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# Saturated vs. Unstaurated

- □ Saturated : Effective stress ( $\sigma$ - $u_w$ ) controls behavior
- □ Unsaturated : Net stress ( $\sigma$ - $u_a$ ) and Matric suction  $(u_a u_w)$  control behavior
- Have seen cut slopes that are steeper than we would allow but they are stable. Why?

Their strength is not being governed by effective stress parameters (c',  $\phi'$ ) but unsaturated shear strength parameters.



#### (from Anderson and Ogunro, 2008)





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# Soil Water Characteristic Curve (SWCC)



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## Pressure Plate Test (ASTM 2325)



(NC State University Soils Lab)

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# **Estimation of SWCC**

- Experimental determination of SWCC is generally difficult, time-consuming and relatively expensive.
- □ SWCC could be reasonably estimated from :
  - Fredlund et al model (2002) : grain size distribution
  - Zapata et al model (1999) : grain size distribution (D60), Plastic Index, % 200 passing
  - SoilVision : a database system for Saturated/Unsaturated soil properties for 6,200 soil samples (98% of them have a SWCC measured in the lab)
  - NCHRP 9-23a : a national catalog of subgrade SWCC default inputs for use with MEPDG

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## **Prediction Methods**

• Fredlund et al.'s approach (1996)

$$\tau_{f} = c' + (\sigma_{n} - u_{a}) \tan \phi' + (u_{a} - u_{w}) [(\theta^{\kappa})(\tan \phi')]$$
  
where,  $\kappa = -0.0016 \cdot I_{P}^{2} + 0.0975 \cdot I_{P} + 1$ 

• Vanapalli et al.'s approach (1996)

$$\tau_f = c' + (\sigma_n - u_a) \tan \phi' + (u_a - u_w) [(\tan \phi') \left(\frac{S - S_r}{100 - S_r}\right)]$$

#### • Khallili and Khabbaz model (1998)

$$\tau_{f} = c' + (\sigma_{n} - u_{a}) \tan \phi' + (u_{a} - u_{w})_{f} [\chi(\tan \phi')]$$
where,  $\chi = \left(\frac{(u_{a} - u_{w})_{f}}{(u_{a} - u_{w})_{b}}\right)^{-0.55}$  for  $(u_{a} - u_{w}) > (u_{a} - u_{w})_{b}$ 
 $\chi = 1$  for  $(u_{a} - u_{w}) < (u_{a} - u_{w})_{b}$ 

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# Kim and Borden Study (2011)

- Each of the procedures was developed based on limited experimental data obtained from a few soils
- Comparisons between measured and predicted values of unsaturated shear strength are presented for different soil types (sandy soil, low plasticity soil, silts, etc.)
- Shear strength data of fifteen soils published in the literature (soils A thru O)
- o Net normal stress (0-200kPa)
- Matric suction (0-1500kPa)





(Kim and Borden, 2011)

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# APPLICATION OF UNSATURATED SOIL SHEAR STRENGTH

# **PROJECT SUMMARY**

Project : Art Commons at University of North Carolina

Location : Chapel Hill, North Carolina

Shoring Method : Temporary Soil Nail Wall

Soil Description : Silty SAND or Clayey Sandy SILT



## **PREPARATION OF SUBSURFACE INFORMATION**

- 1. Five additional soil borings were done.
- 2. Soil samples were collected from various depths at boring locations.
- 3. Additional tests were performed on sampled soils.
- 4. Locations of all nearby utilities were carefully reviewed.

## **GRAIN SIZE DISTRIBUTION CURVE OBTAINED**





SOILVISION is a knowledge-based database software including unsaturated soil data on over 6,200 soil samples. 98% of these soil samples have a soil-water characteristic curve measured in a laboratory. These data are used to estimate unsaturated soil properties.



#### **SHEAR STRENGTH PREDICTION METHODS**

• Fredlund et al.'s approach (1996)

$$\tau_{f} = c' + (\sigma_{n} - u_{a}) \tan \phi' + (u_{a} - u_{w}) [(\theta^{\kappa})(\tan \phi')]$$
  
where,  $\kappa = -0.0016 \cdot I_{p}^{2} + 0.0975 \cdot I_{p} + 1$ 

• Vanapalli et al.'s approach (1996)

$$\tau_f = c' + (\sigma_n - u_a) \tan \phi' + (u_a - u_w) [(\tan \phi') \left(\frac{S - S_r}{100 - S_r}\right)]$$

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 $\chi = 1$  for  $(u_{a} - u_{w}) < (u_{a} - u_{w})_{b}$ 

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## **COMPARISON OF TOTAL COHESIONS OBTAINED**

- per Fredlund et al.'s approach  $\rightarrow$  14.5 kPa
- per Vanapalli et al.'s approach  $\rightarrow$  14.5 kPa
- Khallili & Khabbaz's approach  $\rightarrow$  14.6 kPa

Some soils showed much great differences in total cohesions calculated from three approaches.

#### **CONSTRUCTING TEMPORARY SOIL NAIL WALL**





#### **AERIAL PHOTO OF PROJECT SITE AFTER COMPLETION**



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# **PROJECT SUMMARY**

Project : Wake County Parking Deck

Location : Raleigh, North Carolina

Shoring Method : Temporary Soil Nail Wall

Soil Description : Silty SAND or Sandy SILT

#### PLASTIC COVER AND SUPPLEMENTAL DRILLED SOIL NAIL



#### **ENCOUNTERING ROCK DURING DRIVEN SOIL NAIL INSTALLATION**





## **TENSIOMETER**

- 1. Negative pore-water pressure in soil can be directly measured.
- 2. The measured negative porewater pressure is numerically equal to the matric suction when the pore-air pressure is atmospheric (i.e.,  $u_a = 0$ ).
- The measuring capacity is limited to 100 kPa.

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#### **USE OF TENSIOMETER TO MEASURE ACTUAL MATRIC SUCTION**



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#### **USE OF TENSIOMETER TO MEASURE ACTUAL MATRIC SUCTION**



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### SHORTCOMINGS FOUND DURING THIS PRACTICE

- 1. How can the Soil Water Characteristic Curve obtained from SOILVISION software be confirmed for site specific soils?
- 2. How can moisture content (or matric suction) be confirmed during the project life?
- 3. Which shear strength prediction method is most appropriate to use?



# **CONCLUSIONS**

- Unsaturated soil shear strength properties estimated with information from additional soil tests and SOILVISION software have been used to design temporary soil nail wall.
- 2. Special care needs to be taken for control of natural moisture content (or matric suction) in soil (*i.e.* surface water run-off, ground water and etc.).
- 3. Studies on shortcomings found during this projects should be explored for more confident and wider use.

# Thank you!



#### **CONTACT**

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